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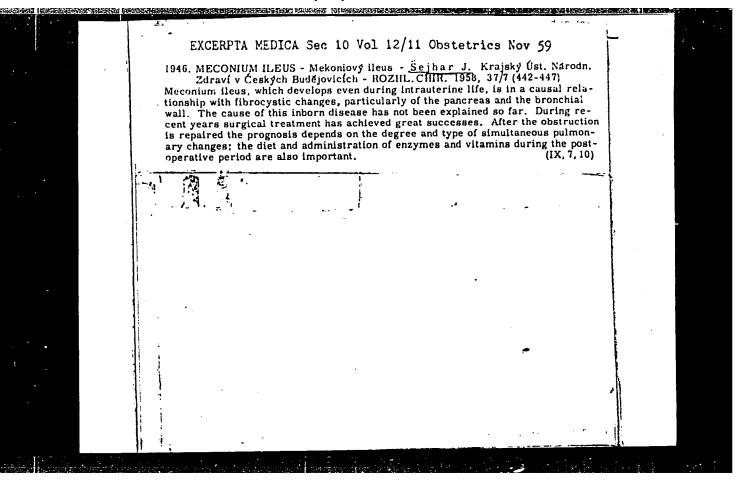
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theory)

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1. Krajska nemocnice v Ceskych Budejovicich, chirurgicke oddeleni, prednosta doc. dr. Jiri Sejhar, neurologicke oddeleni, prednosta primar dr. Vlad. Loucka, pat. anat. oddeleni, prednosta primar dr. Alois Sebek.

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(HERNIA INGUINAL compl) (APPENDIX dis)

SEJHAR, Jiri

CZECHOSLOVAKIA

MD

Docent, MD

Director of the Surgical Department of the Regional Hospital at Ceske Budejovice

Prague, Prakticky Lekar, No 21, Nov 62, pp 900-905

"Notes of an Endocrinologist and Surgeon on Strumectomy"

Co-author:

VACHA, Emil, MD, Chief physician of the Endocrinological Department of the Regional Hospital at Ceske Budejovice

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1. Transporta, Research Worksite, Prague.

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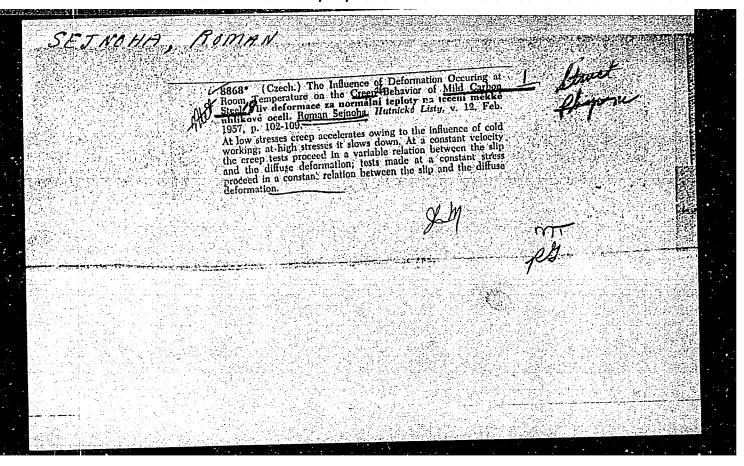
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SEJNOHA, R.

The production of oil pipes having a high yield point. p. 86. (Eutnik, Vol. 7, No. 3, Mar 1957, Praha, Czechoslovakia)

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3200E., 3.

"pelection of the chemical composition of steel for the grade-D casings of horing machinery."

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SEJNOHA, R.

TECHNOLOGY

PERIODICALS: HUTNICKE LISTY Vol. 13, no. 10, Oct. 1958

SEJNCHA, R: SMID V. Use of carbon stell in the manufacture of heat-treated

API-E boring tubes. p. 878

Monthly List of East European Accessions (EEAI) LC Vol. 8, No. 5
May 1959, Unclass.

CZECH/34-59-8-16/16

AUTHOR: Sejnoha Roman, Candidate of Technical Sciences, Engineer

TITLE: Use of Mn-V Steel for Large-size Forgings (Reports on

Czechoslovak Metallurgical Research, Ročník 3, Nr 8, 1959)

PERIODICAL: Hutnicke listy, 1959, Nr 8, pp 743 - 748

ABSTRACT: The work described in this paper deals with investigations of cracks which occur in the manufacture of a large number of forged separators made of Mn-V steel. A sketch of the separator is reproduced in Figure 1. It was forged from a 43-ton ingot; its average body diameter was 1 400 mm. The ingots contained 0.23% C, 1.10% Mn and 0.20% V. steel was produced in some cases in basic open-hearth furnaces; in other cases, it was produced in electric furnaces. The forged separators weighed 25 tons each. The process of manufacture of these forgings is described and also the results obtained on the effect of heat treatment on the micro structure. Investigation on a considerable number of these forgings showed that there is a close relationship between the vanadium content of the steel and the deterioration of the plastic properties at the edges of the forging. Furthermore, highly-developed

Card1/3

CZECH/34-59-8-16/16 Use of Mn-V Steel for Large-size Forgings (Reports on Czechoslovak Metallurgical Research, Ročník 3, Nr 8, 1959)

dendritic non-uniformities were detected in the ingot and these non-uniformities remained very stable during the process of forging; even a comparatively high degree of deformation (upsetting and re-forging with a degree of deformation of 5.5) could not eliminate these nonuniformities. It was also found that there was a weakening of the coherence of the primary grain boundaries. The author recommends that for large forgings for which the degree of deformation cannot be made very high, the use of vanadium-containing steel is not advisable since it is difficult to prevent in such steel the formation of the here mentioned defects. For such purposes, steel should be chosen which has a minimum vanadium content or in which the vanadium is substituted by other substances. Acknowledgements are made to Engineer Jiří Tichý and to the Metallographic Laboratory of NHKG.

Card 2/3

Use of Mn-V Steel for Large-size Forgings (Reports on Czechoslovak Metallurgical Research, Ročník 3, Nr 8, 1959)

There are 15 figures, 3 tables and 6 references, of which 4 are Czech, 1 German and 1 English.

ASSOCIATION: NHKG, Ostrava-Kuntice

SUBMITTED: March 20, 1959

Card 3/3

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"Improving mechanical proporties of standardized love tules by themes in hest trustment."

Hubnik. Praha, Czechoslovakia. Vol. 9, no. 3, tar. 1959

Monthal List of East European Accessions (EEAL), LD, Vol. 8, No. 6, Jun 59, Unclas

SECTIONA, R.

Research of material for oil-casing pipes with the minimum yield point of $90~{\rm kg/cm}^2$. p. 829.

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Uncl.

25639 2/046/61/000/002/003/004 D007/D102

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1573,2808,2708

AUTHORS:

Seinoha, Roman, Engineer, Candidate of Sciences, and

Rohan, René, Engineer

TITLE:

Weldability of hardened and low-tempered 13 MnSiCr

steel

Zváračský sborník, no. 2, 1961, 212-228

TEXT: The article describes welding tests performed with seamless pipes (outside diameter 168 mm, wall thickness 11 mm) made of pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm, wall thickness 11 mm) made of the pipes (outside diameter 168 mm) made of the pipes (outside diameter 16 PERIODICAL: hardened and low-tempered 13 MnSiCr steel, using E 44.72 and E 44.83 hardened and low-tempered 13 MnSiCr steel, using E 44.72 and E 44.85 ferritic-pearlitic electrodes, and E 380 austenitic electrodes. The steel contains 0.13% C, 1.30% Mn, 0.60% Si, 1.40% Cr, and a maximum of 0.035% P and 0.035% S. It has, after hardening and low-temperature tempering (at 200°C), a yield point of 98 kg/mm², a strength of 112 kg/mm² and a ductility of 15% in 2". The purpose of the tests was to investigate the influence of welding on the hardness and notch toughness of the weld joint, and to determine the originating microstructures. In the first test series, soft carbon-steel ing microstructures. In the first test series, ing microstructures. In the first test series, soft carbon-steel

Card 1/4

Z/046/61/000/002/003/004 DO07/D102

Weldability of hardened....

pipe connections were lap-welded onto the 13 MnSiCr-steel pipes. The second test series was performed according to a modification of the VUS 2S weldability-testing method as described by J. Cabelka (Ref. 9: Zváračský sborník 1955, vol. 4, no. 1, 5-45), whereby two halves of an axially-cut 13 MnSiCr-steel pipe were joined by a straight weld. All three above electrode types were used in the first test series, and the E 44.72 and E 44.83 electrodes were used in the second test series. The E 44.72 electrodes with an acid jacket, and the E 44.83 electrodes with a basic jacket, have a minimum strength of 44 kg/mm², and the E 380 electrodes (containing 5% Mn, 18% Cr, 8% Ni, and 0.15% Ti) have a strength of 60 kg/mm², a ductility of 35% (in 5 D), and a notch toughness of 12 kgm/cm.

In the first test series the welds were made with one or two hoods. In the first test series, the welds were made with one or two beads, either normally or by back-stepping, without preheating or postheating. In the second test series, two-bead welds were made. It was found in regard to the martensitic and bainitic transformation temperatures, which are essential for the weldability and tendency to crack formation, that the 13 MnSiCr steel has a very advantageous

Card 2/4

25630

Z/046/61/000/002/003/004 D007/D102

Weldability of hardened...

chemical composition due to its low C content and its alloying components which strongly lower the temperature of bainitic transformation. The notch toughness of the weld metal was higher with the E 44.83 electrodes than with the E 44.72 electrodes, and was highest (12 kgm/cm² at +20°C) with the austenitic electrodes. Although part of the transition zone has a martensitic structure, it retains its high notch toughness and resistance to crack formation due to the rather low C content of the parent metal. However, the tests showed that the strength in the transition zone dropped to 70 kg/mm². This points to the necessity of alloying the 13 MnSiCr steel by such points to the necessity of alloying the 13 MnSiCr steel by such points to the necessity of alloying the 13 mnSiCr steel by such points to the necessity of alloying

Card 3/4

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Weldability of hardened...

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ASM 1956, vol. 48, 51-85; C. L. M. Cottrell, Journal of the Iron and Steel Institute 1953, vol. 174, no. 1, 17; G. F. Comstock, Titanium in Iron and Steel, J. Wiley, New York, 1955,

ASSOCIATION: VZÚ NHKG Ostrava.

Card 4/4

Z/034/61/000/003/001/011 E073/E535

AUTHORS: Sejnoha, Roman, Engineer, Pavelka, Frantisek, C.Sc.-

Industrial Mathematics

TITLE: Toughness of Mn-Si-Cr Steels

PERIODICAL: Hutnické listy, 1961, No.3, pp.153-158

The authors carried out statistical correlation analysis of the results of notch impact tests obtained on TEXT: Mn-Si, Mn-Cr and Mn-Si-Cr steels from nineteen heats after quenching, followed by tempering at temperatures of 200 to 650°C. The contents of the individual elements were within the following limits, in %: 0.14 to 0.33 C, 0.85 to 1.61 Mn. 0.32 to 1.20 Si, O to 1.89 Cr. 0.018 to 0.029 P. 0.023 to 0.036 S. The heats were produced in a 100 kg high frequency furnace with a basic lining, deoxidation was effected solely with ferromanganese or ferro-The cast ingots, weighing silicon without using aluminium. 100 kg, were forged into 70 x 70 mm cross-section bars and these were again forged into 20 mm diameter rods. From these rods, blanks of 14×14 mm cross-section were rough machined for notch impact specimens and also blanks of 14 mm diameter were produced for tensile tests. The rough machined blanks were austenized for Card 1/10

Toughness of Mn-Si-Cr Steels

Z/034/61/000/003/001/011 E073/E535

30 min at the temperature $A_{c_3} + 50^{\circ}C_{+}$ quenched in oil and

tempered for 30 min at 200 to 650°C. After tempering, the specimens were cooled in air and for the tempering temperatures 500 to 650°C cooling was also in water. The tensile specimens were tempered at 200°C and ruptured at +20°C; the determined strength values were used as a check of the quenching process and are entered in Fig.l as a function of the C content (the range between the two curves relates to 99.9% martensite hardening. From the 14×14 mm blanks. Mesnager specimens were produced which For determining the influence of C, Mn, were fractured at +20°C. Si and Cr on the impact strength and for deriving the equations expressing these influences a statistical correlation is necessary. The most favourable mathematical solution is by using determinants, which is practically applicable only for determining the simultaneous influence of three elements and, therefore, calculation of the influence of the elements on the impact strength was subdivided into two stages. In the first stage, the influence of $C_{\mathfrak{g}}$ Mn and Si was calculated for steels with a chromium content of about 1,5%, disregarding the fluctuation of about 0,12% in the Cr Card 2/10

Toughness of Mn-Si-Cr Steels

Z/054/61/000/003/001/011 E073/E535

It was found that the influence of Mn on the impact strength is insignificant, regardless of the tempering temperature. Therefore, in the second stage the influence of C, Si and Cr was investigated (for 19 heats), assuming a constant manganese content in spite of the fact that it actually varied between 0.95 and The relation between the chemical composition and the 1.61%。 impact strength is summarized by the plots, Figs. 2 and 3 in which the coefficients for C. Si and Cr are expressed in percent of the absolute term pertaining to the appropriate temperature; the values for Mn are not plotted, since they did not exceed +10%, It can be seen from these plots that carbon has a highly unfavourable effect at low tempering temperatures, particularly at about 300°C. Above 400°C the effect of carbon is less unfavourable. The unfavourable influence of carbon in the low temperature range is compensated by silicon, the coefficients of which have a characteristic which is roughly opposite to that of the carbon coefficient; at low temperatures its influence is favourable with a maximum of the coefficient at about 350°C; above 400°C the silicon coefficient has a negative value. The coefficient of chromium has a monotonous characteristic, dropping from positive values at the lower tempering temperatures to Card 3/10

Toughness of Mn-Si-Cr Steels

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negative values at medium and high tempering temperatures. The absolute term will be higher after fast cooling from high tempering temperatures than it is after cooling in air; the opposite is true for the coefficient of carbon and silicon. However, there is no difference between chromium and manganese. Consequently, at lower C and Si contents there will be great differences between the impact strength values after quenching in water and in air and the difference will decrease with increasing C and Si contents. This influence of Si and C is illustrated by Fig. 4. The range of low temperature temper brittleness and the drop in impact strength in this range can be expressed by the following equations:

$$T_{min} = 265 + 107 \text{ Si} + 22 \text{ Cr}$$
 (19)

$$\Lambda R = 25 - 32 \text{ Si} + 30 \text{ Cr}$$
 (20)

where T is the temperature. °C, at which the impact strength is at a minimum, ΔR - drop in impact strength expressed in percent of R_{200} °C° SiCr - Si and Cr contents in percent.

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Toughness of Mn-Si-Cr Steels

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Fig. 5 shows the characteristic of the impact strength of four typical Mn-Si-Cr steels calculated by means of the equations derived in this paper. It is concluded that the main advantages of Mn-Si-Cr steels is their high impact strength combined with high strength after hardening, followed by low temperature tempering. The favourable effect of Cr and particularly of Si compensates the effect of C on the notch impact strength so that the C content and thus the strength can be increased whilst maintaining a satisfactory impact strength. Simultaneously, Cr, and particularly Si, increase the temper brittleness temperature and thus extend the range of satisfactory impact strength. For high tempering temperatures, steels with lower C contents and not too high contents of Si and Cr should be used in which the impact strength does not drop below tolerable limits. The main effect of the manganese is in increasing hardenability; for the entire range of the investigated tempering temperatures, manganese had neither pronounced favourable nor unfavourable effect on the impact strength. There are 5 figures, 17 tables and 11 references, 2 Czech and 9 non-Czech.

ASSOCIATION: VZÚ NHKG, Ostrava Card 5/10

SEJNOHA, Roman, inz., C.Sc.

Oil pipes with a high yield point in tension. Sbornik skol ban 8 no.3:345-354 '62.

1. Vyzkumny a zkusebni ustav, Nova hut Klementa Gottwalda, Ostrava - Kuncice.

SEJNOHA, Roman, inz., C.Sc.; ROHAN, Rene, inz.

Weldability of hardened and low tempered 13 MnSiCr steel. Zver sbor 10 no.2:212-228 *61.

l. Vyzkumny a zkusebni ustav, Nova hut Klementa Gottwalda, Ostrava.

Z/034/61/000/005/002/010 E073/E535

AUTHOR: Sejnoha, Roman, Engineer, Candidate of Science

TITLE: Influence of vanadium and titanium on the properties of

steel for high strength tubes

PERIODICAL: Hutnicke listy, 1961, No.5, pp.351-355

TEXT: One of the tasks of the Czech metallurgical industry is the manufacture of tubes for deep drilling for oil. This steel was developed on the basis of the results obtained with the experimental steel 13MnSiCr with a yield point of 98 kg/mm². The aim of the work described in this paper was to compare the influence of vanadium and titanium on the properties of the investigated steel in the quenched and tempered states. The compositions of the experimental melts in percent are given in Table 1.

Steel C Mn Si Cr Mo V Ti Ni Al P S

20MnSiCrMoV 0.19 1.32 0.85 1.28 0.29 0.15 0.01 0.12 0.035 0.020 0.015 20MnSiCrMoTi 0.18 1.20 0.92 1.16 0.28 0.02 0.10 0.08 0.035 0.016 0.016 0.016 0.016 0.016

Influence of vanadium and titanium ... Z/034/61/000/005/002/010 E073/E535

The melt with titanium as well as that with vanadium were deoxidized with aluminium, 1 kg/ton. From each, an ingot weighing 3850 kg was produced. These were rolled into billets of 140 mm diameter and then into tubes of 5 9/16" x 11 mm. as-rolled state, the strength (calculated in terms of hardness) was 123 kg/mm² for the melt with vanadium and 112 kg/mm² for the melt The tubes were then heated to 930°C (50°C above Ac3), water quenched by means of a ring-shaped spray with a speed of movement during quenching of about I m/min. The tubes were then cut into segments 250 mm long and about 80 mm wide. of these segments were tempered for 30 min at temperatures between 100 and 650°C with furnace cooling, air cooling or water cooling; some of the segments were not tempered at all. Some of the segments were annealed at 750°C for 30 min, furnace cooled, straightened in a press, heated to 900°C for 30 min and water quenched and then tempered at 200, 400 and 600°C. Analysis of the results shows that for the given types of steel, vanadium addition is undoubtedly more favourable than addition of titanium if the steel is to be used in the high strength state. By tempering of quenched tubes of this steel at 300°C, the following properties Card 2/6

Influence of vanadium and titanium.. Z/034/61/000/005/002/010 E073/E535

can be achieved: a strength of 148 kg/mm² with a yield point of 126 kg/mm²; elongation of 10.5% for 5D and 17.5% for 2"; an impact strength of 8.5 kgm/cm² at +20°C and 6.5 kgm/cm² at -70°C. The obtained results show that vanadium brakes the drop in strength caused by tempering; between 550 and 600°C the drop in strength is braked completely and only tempering above 600°C results in a rapid decrease in strength. Titanium alloyed steels show a rapid drop in strength above 400°C; no secondary hardness was observed. Steel with vanadium has a more pronounced tendency to high temperature temper brittleness than steel with titanium. After low temperature tempering, steel with vanadium has a higher impact strength, particularly at low temperatures, than steel with titanium. After high temperature tempering, the position is reversed. at more elevated test temperatures is the quality coefficient of titanium alloyed steel higher. Steel with Ti has a lower content and a better distribution of the impurities and also a higher impact strength in the transverse direction. For tubes made of the steel 20MnSiCrMoV and tempered at 300°C after quenching, a yield point above 120 kg/mm² was achieved and on 2" tubes a contraction above 50% was achieved. Acknowledgments are expressed to Card 3/6

Influence of vanadium and titanium.. Z/034/61/000/005/002/010 E073/E535

Engineer Hladky and Engineer Lubovsky of VZKG and to Engineer Kalivoda, Engineer Hyspecky, J. Socha and Engineer Togner of NHKG who participated in the experiments. There are 13 figures, 1 table and 16 references: 9 Soviet-bloc and 7 non-Soviet-bloc.

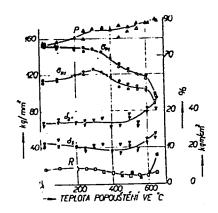
ASSOCIATION: VZU NHKG, Ostrava SUBMITTED: February 7, 1961

Fig.1. Legend

Influence of the tempering temperature on the mechanical properties of quenched tubes from the steel 20MnSiCrMoV.

kg/mm
2
) vs. tempering temperature, kgm/cm 2) °C

Card 4/6



Z/054/61/000/007/002/007 E075/E335

AUTHOR Sejnoha, Roman, Engineer, Candidate of Sciences

TITLE: Properties of a New Economy Steel 13 MnSiCr for Heattreatment (Quenching and Tempering)

PERIODICAL: Hutnické listy, 1961 No. 7, pp. 476 - 483

published) the author considers the potentialities of MnSiCr steels from the point of view of toughness and shows the possible applications of a steel of this type with a low carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, carbon content. In an earlier paper (Ref. 2 - Hutnické listy, with carbon content, and levelopment with the development of 15% (I industry, with carbon content, and an average composition of 0.13% C. 1.30% Mn. 0.60% Si and listed has a minimum yield point of 98 kg/mm, a minimum strength steel has a minimum yield point of 98 kg/mm, a minimum strength of 112 kg/mm, a minimum clongation of 15% (2" tube) and a satisfactory impact strength even after this steel had a satisfactory impact strength even after tempering at temperatures up to A (Abstracter's note: a later, card 1/5

Z/034/61/000/007/002/007 E073/E335

Properties of was-

more-detailed paper on this steel has been published in Hutnické listy, 1961, No. 5, pp | 351 + 355). Information on a similar steel has been published by V.K.Barziy et al (Ref. 5 · Stal* 1959 No. 5, pp. 456-439). The aim of the here described work was to determine the main properties of this 13 MmSiCr steel after various types of heat treatment and to study the influence of aluminium on its properties. A favourable influence on this steel is attributed to the aluminium used for its deoxidation, particularly as regards the toughness and the tendency to embrittlement of quenched and tempered steels. The welding of this steel are dealt with in another paper (published in Avaracsky sborník, 1961, No.2). Material from an earlier produced heat and from 10 experimentalheats was used in the experiments. The compositions fluctuated between the following limits: 0.15 - 0.16% C, 1.35 - 1.44% Mn, 0.52 - 0.70% Si, 1.40 - 1.50% Cr and 0.025 - 0.029% S. To study the influence of aluminium the quantity of aluminium used for deoxidation was made to vary between 0 and 2 kg/t. Various P contents between 0.024 and 0.122% were used to achieve various degrees of high-temperature temper brittleness. Ingots of Card 3/5

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Z/034/61/000/007/002/007 E073/E335

Properties of

100 kg were produced, which were forged to 70 x 70 mm rods and then to 20 and 30 mm rods. These heats were used for determining the transformation characteristics and the main mechanical properties of the steel and the influence of Al and P on its properties. Hardenability tests were made after austenising at 900 °C for 30 min. From the obtained hardness values, microstructure and the calculated transformation temperatures, a diagram of the anisothermal decomposition of austenite of the investigated steel was constructed. The influence was established of the heat-treatment conditions (speed of cooling from the austenisation temperature and tempering time) on the mechanical properties of this steel. It was found that the yield point of the quenched steel increased with increasing tempering temperatures up to 400 °C. Up to this temperature there is hardly any drop in strength; above this temperature the strength decreases fairly sharply.
Up to 400 °C the ductility drops slightly: however, at higher temperatures it increases sharply. Due to its low carbon content the steel 13 MnSiCr should be free of Card 3/5

Z/034/61/000/007/002/007 E073/E335

Properties of

low-temperature temper brittleness. The drop in the impact strength at 20 °C was quite insignificant for this range of temper brittleness (which, due to the effect of Si, is shifted towards higher temperatures). However, there is a pronounced increase in the critical brittleness temperature, which indicates that, to a certain extent, low-temperature temper brittleness does develop in this steel. Due to its grain-refining effect the Al had a favourable influence on the properties of the steel, particularly on the low- and high-temperature temper brittleness. However, it does reduce slightly the strength in the high-temperature tempered state and a decrease in ductility was observed for Al contents of 0.02 - 0.03%. P lowers the impact strength under any condition of heat-treatment. It also affects the level of the critical brittleness temperature and the high-temperature temper brittleness. P also lowers considerably the ductility. The influence of P was only partly offset by the grain-refining effect of the Al. In the high-temperature tempered state, P improved the strength properties (by its effect on the strength of the Card 4/5

Z/034/61/000/007/002/007 E075/E335

Properties of

ferrite). The steel 15 MnSiCr has a high hardenability; in spite of its high strength it has a satisfactory ductility and, particularly, a satisfactory impact strength. Therefore, the author recommends using this steel not only for oilindustry tubes but also for machinery where a high-strength There are 21 figures, 4 tables and material is required. The four latest 6 Czech and 21 non-Czech. 27 references: English-language references quoted are: Ref. 9 - H. Steven and A.G. Haynes - J. Iron and Steel Institute, 183, 1956, No. 4, pp. 349-359; Ref. 12 - R.H. Aborn - Trans. ASM, 1956, Vol. 48, pp. 51-85; Ref. 17 - H. Muir, B.L. Averbach and M. Cohen - Trans. ASM, 1955, Vol. 47, pp. 580-407; Ref. 25 - B.L. Bigs - J. Iron and Steel Institute, 192, 1959, No. 4, pp. 361-377.

ASSOCIATION: VZÚ NHKG, Ostrava SUBMITTED: November 28, 1960

Card 5/5

SEJNOHA, Roman, inz., C.Sc.

Increasing the notch toughness of steel for railroad car axles. Hut listy 16 no.12:862-865 D '61.

1. Vyzkumny a zkusebni ustav, Nova Hut Klementa Gottwalda, Ostrava-Kuncice.

(Car axles) (Railroads) (Steel)

SECTIONA, Noman, doc. inz. 630.

High-strength low-earmn steel. Sbor VSB Ostrava 9 no.3:
311-334 '63.

1. Vysoka skola banska, Ostrava.

SEJNOHA, Roman

Properties of manganese-silicate-chromium steels and their improvement by addition of aluminum. Hut listy 18 no. 12: 859-865 D 163.

1. Vysoka skola banska, Ostrava.

SEJNCHA, Roman, doc. inz. DrSc.; HULICIOVA, Zdenka

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Carbides in the hardened and tempered manganese-silicon-chromium steel with a low carbon content. Sbor VSB Ostrava 10 no.3:337-351 '64.

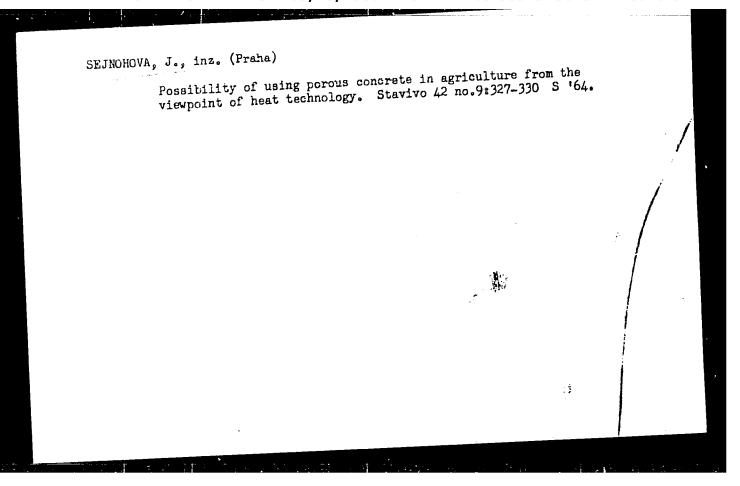
1. Higher School of Mining, Octrava (for Sajnoha). 2 Research and Testing Institute of the nova hut Klementa Gottwalda National Enterprise, Ostrava-Kuncice (for Huliciova). Submitted June 5, 1963.

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Effect of metallurgical factors on the corrosion of hot-water pipes. Sbor VSB Ostrava 10 no.3:361-370 '64.

1. Chair of Metal Science and Thermal Processing of the Higher School of Mining, Ostrava. Submitted September 11, 1963.

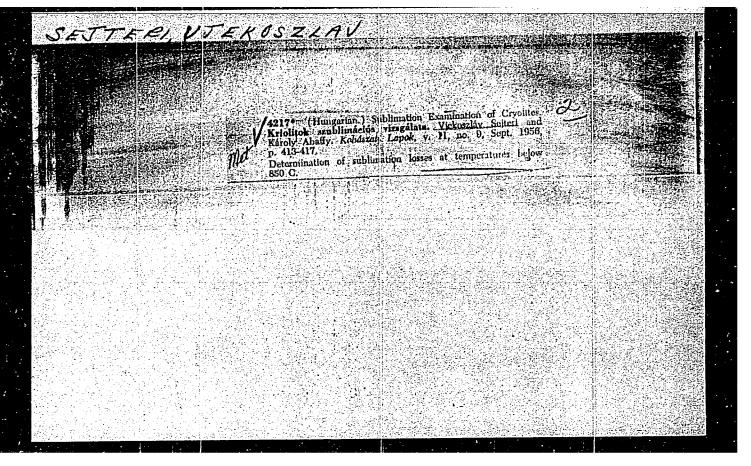
| ACCESSION NR: AP50 | GNP(t) JD GZ/0034/64/000/010/0715/0720 |
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| | |
| AUTHOR: Sejnoha, F Lubos (Engineer) | bean (Engineer, Doctor, Candidate of sciences); Hyspecky. |
| TTTE: Use of high | -speed reheating for the heat treatment of tubes |
| 경화가 많다 하는 학교 회사를 받는 것 같다. | 를 보통하다는 하다. 전환경 10명이 되지는 하를 모르겠다면 하면 하면 하는 하게 하다. TAS (12명이 등 기본 12명이 12명이 12명이 되었다면 하다. 12명이 12명이 12명이 12명이 1 |
| SOURCE: Hutnicke 1 | listy, no. 10, 1964, 715-720 |
| | metal heat treatment, hardness, solid mechanical property |
| 이 없는 하는 하는데 그는 그림을 다시하는데 하는데 이 한 이 문문을 된다. | problems concerning austenitization occuring in high-speed yzed. An example is presented to prove that equal hardness perties, resulting from quenching and tempering of tubes, may perties, resulting from the conventional reheating technique |
| and mechanical pro | highed reneating just as of the convenience |
| and mechanical probe achieved by high | 6 figures, 9 graphs, 2 tables. |
| and mechanical probe achieved by high Orig. art. has: ASSOCIATION: Sejne | 6 figures, 9 graphs, 2 tables. Oha - VSB, Ostrava; Hyspecky - VZU HHKG, Ostrava |
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| and mechanical probe achieved by high Orig. art. has: ASSOCIATION: Sejne | h-speed reheating just as by the convenience of figures, 9 graphs, 2 tables. Oha - VSB, Ostrava; Hyspecky - VZU HHKG, Ostrava ENCL: OO SUB CODE: 191, AS |



SEJPA, C. - Kridla Vlasti No. 13, June 1955

Care of parachutes in the winter season. p.302.

SO: Monthly List of East European Accessions, (EEAL), LC, Vol. 4, No. 9, Sept. 1955, Uncl.



SEJUT, Zhimiew

Analysis of the preision of altimetric measurements of inaccessible points performed by the spatial intersection method for the purpose of testing the deformations for construction measurements. Good i kart 10 no.3/4:229-260 161.

"APPROVED FOR RELEASE: 08/23/2000

CIA-RDP86-00513R001547710010-5

s/035/62/000/010/092/128 VO01/V101 inalysis of accuracy of height measurements of inaccessible points by the space intersection method for investigating deformations Sejut, Zbigniew AUTHOR: PERIODICA:: Referativnyy zhurnal, Astronomiya i Geodeziya, no. 10, 1962, 17, 229 Referatively Engreal, Astronomiya 1 Geometrya, no. 10, 1902, 11, abstract 10G8% ("Geod. i kartogr.", 1961, v. 10, no. 3 - 4, 229 - 250 polich. TITLE: 250, Polish; French and Russian summaries) The plan and height position of two points located in one vertical The plan and neight position of two points located in one vertice the triplane was determined from triangle vertices fixed on the locality; plane was determined from triangle vertices with steel wines and the angles will be applied to the steel wines and the angles will be applied to the steel wines and the angles will be applied to the steel wines and the angles will be applied to the steel wines and the angles will be applied to the steel will plane was aptermined from triangle vertices lixed on the locality; the triangles with steel wires and the angles with
angles sides, 24 - 32 m long, were measured with steel wires and to a shown
angle sides, 24 - 32 m long, were measured at a height of or is mahove angle sides, 24 - 32 m long, were measured with steel wires and the angles with a m-2 Wild theodolite. The first point was located at a height of ~ 15 m above the ground and the second one at about 1 5 m mo determine the height of the the ground, and the second one at about 1.5 m. To determine the height of the the ground, and the second one at about 1.7 m. To determine the height of the rotation axis of the theodolite tube, three ground marks were leveled, each of ... The respect triangle venter to the respect triangle venter. rotation anis of the theodolite tupe, three ground marks were leveled, each o which was at a distance of ~3 m from the nearest triangle vertex. Leveling which was at a distance of ~3 m from level instrument and invar node which was it a distance of a juniform the hearest triangle vertex. Leveling was performed with a Ni-OO4 precision level instrument and invar rods. The was performed with a NI-UU4 precision level instrument and invar rods. The measurement precision is characterized by the following data: rms error in Card 1/4

s/035/62/000/010/092/128 A001/A101

Analysis of accuracy of ...

measuring triangle angles is $\pm 3^{ec}$.52; rms relative error in measuring triangle sides is 1:371,000, which corresponds to angular error of $\pm 1^{cc}$.71; rms error in determining the mark height amounted to ±0.04 mm on the average. The triangle was adjusted twice: taking into account the weights of measured angles and sides and without this. Divergences in adjusted values of vertex coordinates amounted to 0.7 mm. The results obtained with allowance for weights were adopted for further calculations. Each point to be determined was intersected from the triangle vertices by measuring horizontal and vertical angles in 25 observations. The height of the theodolite tube rotation axis was determined twice: by means of measuring the inclination angle by aiming the tube at a centimeter line of a rod located near the horizon, and by sighting the rod with a horizontal ray. In so far as in intersections the tube sighting axis formed with the horizon different angles, corresponding corrections were introduced into measured horizontal directions. With the aim of a comparison, coordinates of determined points were calculated as dependent on both corrected and noncorrected directions. Practically the same results were obtained. The calculation of coordinates of determined points was checked by means of special nomograms. The heights of intersected points were calculated as weighing

Card 2/4

S/035/62/000/010/092/128 A001/A101

Analysis of accuracy of ...

averages for each intersection. Weights were determined by the formula:

$$p = \frac{1}{m^2}, \quad \text{where } m_H^2 = m_{HR}^2 + m_{H1}^2 + m_{\Delta h}^2.$$

Here $m_{\hat{I}\hat{I}\hat{I}\hat{I}}$ is error in the mark height upon which depends the height of the tube rotation axis, $m_{\hat{I}\hat{I}}$ is error in determining the height of the tube rotation axis, $m_{\hat{I}\hat{I}}$ is error in elevation of the intersected point which is calculated by the formula:

$$m_{\Delta h}^{2} = \frac{t_{x}^{2} \varphi}{\sin^{2}(\alpha + \beta)} \left[\sin^{2} \beta \cdot m_{c}^{2} + \frac{c^{2} \sin^{2} \beta}{\sin^{2} \varphi \cos^{2} \varphi} m_{y}^{2} + c^{2} \sin^{2} \beta \cot^{2}(\alpha + \beta) \cdot m_{\alpha}^{2} + c^{2} \frac{\sin^{2} \alpha}{\sin^{2}(\alpha + \beta)} m_{\beta}^{2} \right].$$

in which α , β are horizontal angles, φ is inclination angle of the sighting axis, c is the length of the base, m φ , m $_{\alpha}$, m $_{\beta}$, m $_{c}$ are respective rms errors. The error values were assumed to be as follows: m $_{\alpha}$ = m $_{\beta}$ = $\pm 15^{cc}$, m $_{\phi}$ = $\pm 9^{cc}$,

Card 3/4

Analysis of accuracy of...

S/035/62/000/010/092/128 A001/A101

 $m_{\rm C}=\pm0.07$ mm, $m_{\rm HR}=\pm0.04$ mm and $m_{\rm Hi}=\pm0.06$ mm; then the rms errors in determining heights of intersected points proved to be, on an average, ±0.8 mm for a point located high and ±0.5 mm for a point located near the horizon. The results of determining the heights of the intersected points were compared with the results of double precision leveling of the same points, and divergences both actual r and limiting $r_{\rm gr}$ were calculated: $r_{\rm gr}=3\sqrt{m_1^2+m_2^2}$, where m_1 and leveling. The actual divergence was greater than the limiting one in one case only. At the end of the article the author analyzes errors in measuring vertical

N. Modrinskiy

[Abstracter's note: Complete translation]

Card 4/4

SEJVL, MIRUSLAV

Theorie a vypocty ozubenych kil. (Vyd. 1.) Praha, Statni nakl. technicke Liyrtsyuty. (The theory and calculations of gears. 1st ed. bibl., diagrs., footnotes, graphs, tables) Vol. 1. (Spur gearing bevel gearing modified gear cutting, gear pumps, root compressors, mathematics of gearing and planetary gearing and differentials) 1957. 555 p.

SO: Monthly Index of East European Acessions (EEAI) Vol. 6, No. 11 November 1957

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Static solutions of composite surface systems by means of the method of double or triple indefinite rule. p. 69. (Strojnoelektrotechnicky Casopis, Vol. 8, No. 2, 1957, Bratislava, Czechoslovakia)

SO: Monthly list of East European Accessions (EE-L) IC, Vol. 6, No. 8, Aug 1957. Uncl.

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Driving mechanisms by W. Lichtenheldt. Reviewed by M. Sejvl. Strojirenstvi 12 no.10:794 10 0 '62.

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Calculation of the set-up of spiral bevel gear generators for optimal transfer of the tool bevel faces. Stroj cas 14 no.1: 37-50 63.

1. Vysoka skola strojni a elektrotechnicka, Plzen.

STACHURA, Jerzy; JORDECZKA, Stanislaw; KIELOCH-SZKODA, Matylda; SEK, Stanislaw.

antenant and to the control of the c

Diagnostic difficulties in pulmonary adenomatosis. Pol. tyg. lek. 19 no.3:86-89 20 Ja*64

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LTSOWSKA, Jadwiga; SEK, Helena

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A case of multiple self mutilations. Neurol. neurochir. psychiat. Pol. 15 no.2:341-344 Mr-Ap 165.

1. Z Kliniki Psychiatrycznej AM w Poznaniu (Kierownik: prof. dr. R. Dreszer).

SEKA, Jaroslav

Experience with a complex plan for the improvement of health conditions of an industrial center. Cesk. zdravot. 4 no.10: 608-609 Oct 56.

andrianiem in the American of the State of t

1. Oddeleni Hygieny prace KHES Hradec Kralove.
(INDUSTRIAL HYGIENE,
in Czech. (Cz))

YUGOSLAVIA/Chemical Technology. Chemical Froducts and Their Applications. Leather, Furs. Gelatin. Tanning Materials. Industrial Proteins.

Abs Jour: Ref Zhur-Khimiya, No 6, 1959, 21966

: Sekac, Mirek Author

: Use of Glass Plates for Glueing Light Tnst Title

Leathers.

Orig Pub: Kozha i obuca, 1953, 7, No 5, 169-172

Abstract: In the order of its derivation from experiments, a method of treatment and formulation of working solutions for conduct ting technological processes which precede drying leathers by glueing them on glass

: 1/2 Card

CIA-RDP86-00513R001547710010-5" **APPROVED FOR RELEASE: 08/23/2000**

- SEKACH, F.M.

Simplified rubber apparatus for rectal mud therapy. Yop. kur., fizioter. i lech. fiz. kul't. 25 no. 6:554-556 N-D '60.

(MIRA 14:2)

1. Iz sanatoriya No. 2 (glavnyy vrach V.Ya. Budilov) kurorta Morshin. (BATHS, MOOR AND MUD) (MEDICAL INSTRUMENTS AND APPARATUS)

ZLOTNIK, E.I.; SEKACH, S.F. (Minsk)

ves tel politica (il liggar op t ble doli). Heli ble bij ble dos

Technic for surgery in arterioscleratic stenosis of the internal caratoid artery of the neck region. Vop.neirokhir. no.2:7-9 162. (MIRA 15:3)

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(ARTERIOSCLEROSIS) (CAROTID ARTERY.—SURGERY)

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Surgical treatment of thrombosis and stenosis of the internal carotid artery. Zhur.nevr.i psikh. 62 no.8:1172-1177 Ag '62.

(MIRA 15:12)

l. Neyrokhirurgicheskoye otdeleniye Belorusskogo nauchnoissledovatel'skogo instituta nevrologii, neurokhirurgii i fizioterapii (dir. Ye.Kalitovskiy), Minsk. (CAROTID ARTERY_DISEASES) (ARTERIOSCLEROSIS) (THROMBOSIS)

ZLOTNIK, E.I., SEKACH, S.F.

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Investigating the oxidizing zone of a blast furnace working under oxygen-enriched blowing (35% oxygen) and using natural gas. Stal! 25 no.8:781-790 S 165. (MIRA 18:9)

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- 2. UJSE (600)
- 4. Theep Breeds
- 7. Maising Alai fat-rumped sheep. bots. zhiv. 15, No. 5, 1953.

9. Monthly List of Russian Accessions, Library of Congress, April 1953, Uncl.

SEKACHEV, VI.

BEZGINOV, I.P., professor-prepodavatel', polkovnik,; VELYUGO, V.M., professorprepodavatel polkovnik, GERASIMOV, A.I., professor-polkovnik, polkovnik,; LEBEDEV, A.I., professor-prepodavatel', polkovnik,; MILYUTENKOV, D.M., professor-prepodavatel', polkovnik,; PROKHORKOV, I.I., professor-prepodavatel', polkovnik,; SEKACHEV, V.I., professorprepodavatel', polkovnik,; SOROKIN, V.N., professor-prepodavatel', polkovnik, : UKHOV, N.E. professor-prepodavatel polkovnik, ; FEDOTOV, B.I., professor-prepodavate1', polkovnik,; SHIRYAKIN, N.V., professorprepodavatel', polkovnik,; SHMRLEV, M.S., professor-prepodavatel', polkovnik,; ANISIMOV, N.I., professor-prepodavatel , polpolkovnik,; BULATOV, A.A., professor-prepodavatel', podpolkovnik,; SIDORENKO, A.A., professor-prepodavatel', podpolkovnik, ; SHKODUNOVICH, N.N., general-leytenant, glavnyy red.; BANNIKOV, M.K., polkovnik, red.; DAVYDOV, F.M., polkovnik, red.; LOZOVOY-SHEVCHINKO, V.M., general-mayor. aviatsii, red.; SHIPOVA, B.V., polkovnik, red.; MOROZOV, B.N., polkovnik, red.; VOLKOVA, V.E., tekhn. red.

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